

SHORT COMMUNICATION

The  $X_2$  proof for weibull's distribution and the anisotropy of an electrical porcelain

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The present work utilized experimental data for strength in bending of a relatively large number (> 500) of specimens of an electrical porcelain. This note is concerned with the applicability of the Weibull model to these data.

Rectangular bars were formed by extrusion under vacuum, using a classical electrical porcelain body comprised of kaolin, ball clay, feldspar and silica †. The bars, after drying, were fired to 1200° C, and held at that temperature for three hours. The fired dimensions of the test bars were about 0.435 cm by 1.0 cm by 5.4 cm. The fired bars were loaded in three point bending, using a mechanical testing machine with a cross/head speed of 0.5 cm/min, to failure (Fig. 1). The apparent porosity of the bars (by ASTM C 20/46) was determined to be 0%; closed pores were observed with examination of fracture surfaces by scanning electron microscopy.

As given by Weibull [1, 2], the cumulative probability of fracture in a non-uniform stress field is:

$$F(\sigma) = 1 - \exp\left\{-\frac{1}{V_0} \iiint_V \left(\frac{\sigma(x, y, z) - \sigma_0}{\sigma_0}\right)^m dx dy dz\right\}, \quad (1)$$

where  $V_0$  is the unit volume (for this case  $1 \text{ cm}^3$ ),  $V = bhL$  is the sample's volume,  $\sigma_1$  is the stress below which there is no fracture, and  $m$  and  $\sigma_0$  are specific parameters of the material. To calculate  $F(\sigma)$ , it is assumed that

$$\sigma_1 = 0, \text{ and since } \sigma(x, y, z) = \frac{4xy\sigma}{Lh}$$

$$\sigma < \frac{3}{2} \frac{PL}{bh^2}, \quad 0 < x < \frac{L}{2},$$

$0 < y < h/2, \quad 0 < z < b$ , then:

$$F(\sigma) = 1 - \exp\left\{-\frac{bhL}{2V_0(m+1)^2} \left(\frac{\sigma}{\sigma_0}\right)^m\right\} \quad (2)$$

The values of  $\sigma$  fell within  $429 \text{ kgf/cm}^2$  (42.1 MPa) and  $813 \text{ kgf/cm}^2$  (79.7 MPa); this interval was divided into 29 parts and the values for  $F(\sigma)$  were calculated at points for  $\sigma_i = (429 + i\Delta\sigma) \text{ kgf/cm}^2$ , where  $\Delta\sigma = 12.8$

and  $i = 0.1, \dots, 30$ . Then  $F(\sigma_i) = n_i^c/N$ , where  $n_i^c$  is the number of samples broken experimentally at a stress equal or less than  $\sigma_i$ , and  $N = 584$  (the total number of samples broken). Since the new variable.

$$\begin{aligned} r_{n_i^c} &= \ln \left\{ \ln \frac{1}{1 - F(\sigma_i)} \right\} = \\ &= \ln \left\{ \ln \left( \frac{N}{N - n_i^c} \right) \right\} \end{aligned} \quad (3)$$

can be linearly dependent of  $\ln \sigma_i = \xi_i$  in accord with (2), it provides a useful evaluation to plot  $r_{n_i^c}$  as a function of  $\xi_i = \ln \sigma_i$  which gives a straight line with some dispersion (Fig. 1). The equation for this straight line, obtained graphically, is:

$$r_{n_i^c} = 14 \xi_i - 92 \dots \quad (4)$$

where  $n_i^t$  is the theoretical value of  $n_i$ ; there is an exact linear relation (4) between  $r_{n_i^c}$  and  $\xi_i$ .

On taking the natural log of equation (2) it can be found that:

$$\begin{aligned} r_{n_i^c} &= \ln \left( \ln \frac{1}{1 - F(\sigma_i)} \right) = \ln \left( \ln \frac{N}{N - n_i^c} \right) \\ &= m \ln \sigma_i + \ln \left( \frac{bhL}{2V_0(m+1)^2 \sigma_0^m} \right) \end{aligned} \quad (5)$$

which allows us to obtain  $\sigma_0 \approx 481 \text{ kgf/cm}^2$  (47.2 MPa) and  $m = 14$ , once (5) is compared with (4). Now the theoretical values for  $n_i^t$  can be calculated from (5) as

$$n_i^t = N \left( \frac{e^{e^c r_{n_i^c}} - 1}{e^{e^c r_{n_i^c}}} \right) \quad (6)$$

where the differences  $\Delta n_i^t = n_i^t - n_{i+1}^t$  and  $\Delta n_i^c = n_i^c - n_{i+1}^c$ , providing the theoretical and experimental frequency curves respectively. The applicability of the Weibull theory may be further evaluated by the  $X^2$  «goodness of fit» test [3]. Using this test the value for  $X^2$  is given by:

$$X^2 = \sum_{i=1}^{30} \frac{(\Delta n_i^t - \Delta n_i^c)^2}{\Delta n_i^t} \approx 44.57 \dots \quad (7)$$

† Overall oxides content of the fired body: 71.9 %  $\text{SiO}_2$ , 22.9 %  $\text{Al}_2\text{O}_3$ , 1.2 %  $\text{CaO}$ , 0.1 %  $\text{MgO}$ , 2.1 %  $\text{K}_2\text{O}$ , 0.6 %  $\text{Na}_2\text{O}$ , 0.7 %  $\text{Fe}_2\text{O}_3$ , 0.5 %  $\text{Tl}_2\text{O}_2$  (by weight).

This value falls in the interval:

$$X_{0.975}^2 = 45.7 > \chi^2 = 44.7 > \chi_{0.025}^2 = 16$$

for 29 degrees of freedom (number of intervals minus 1). A gaussian distribution was also used, but  $X^2 = 180$  eliminated this distribution.

Thus, it is concluded that the Weibull's function (1) gives a representation of the experimental results with a  $X^2$  test corresponding to the 95 % significance level,

giving a better correlation than provided by a gaussian function.

In order to confirm this conclusion a new batch of 55 samples was tested (Fig. 1). But now the sample with  $b = 0.45$  cm,  $h = 1$  cm and  $L = 4.95$  cm. Formula (5) shows that  $m$  is the same with this new configuration in the test, but experiments give  $m = 4.67$  so it is concluded that must be a strong anisotropy in the sample. Investigation in order to check this is at present being experimentally made.

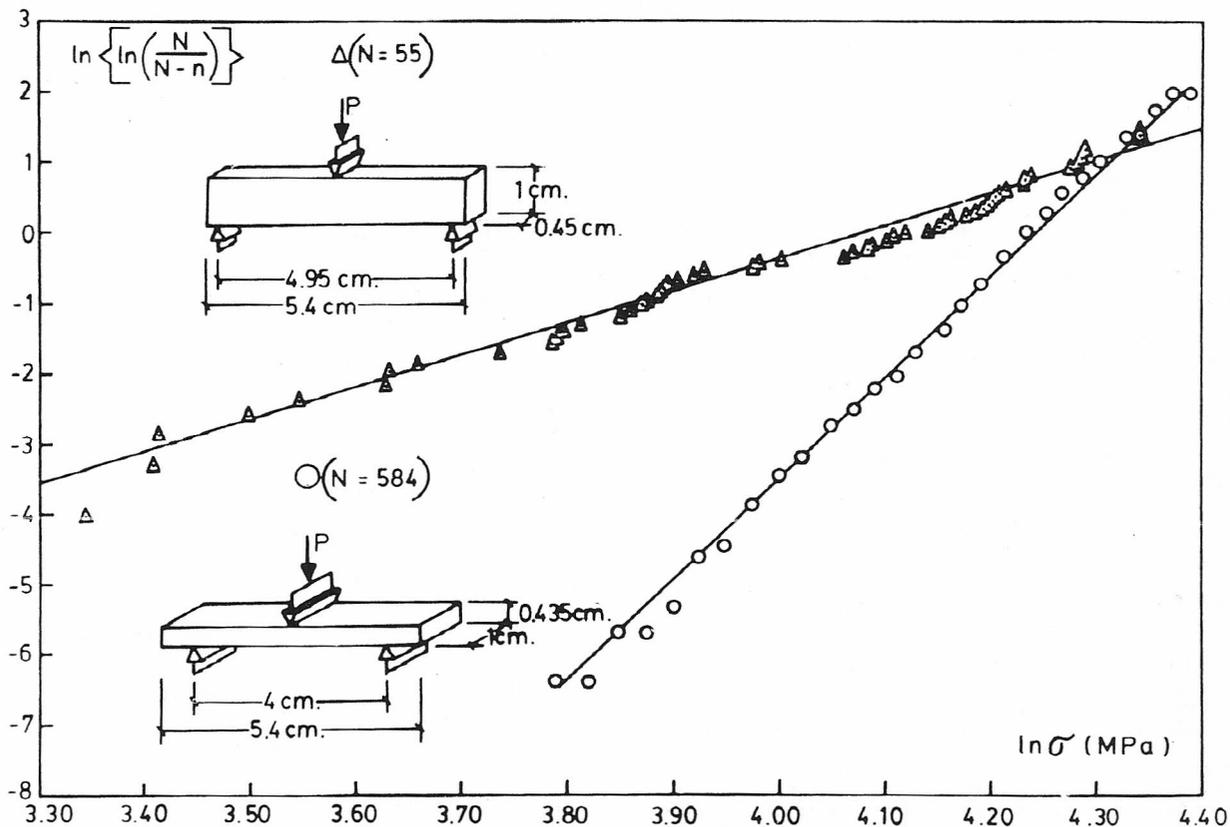


Fig. 1. Dimensions of the samples and Weibull's plot.

REFERENCE

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3. Benjamin, J. R. and Cornell, C. A.: *Probability, Statistics, and Decision for Civil Engineers*, pp. 460-1, McGraw-Hill Book Co., New York, 1970.